WEBB COUNTY DRAINAGE DISTRICT NO. 1

HYDRAULIC AND HYDROLOGIC STUDY (LOMAS DEL SUR & CUATRO VIENTOS SUR)



WCDD BOARDMEMBERS

Ms. Leti Martinez President

MR. AMBROSIO GARZA TREASURER

MS. MARGIE ARCE BOARDMEMBER



SUBMITTED BY:





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1. PURPOSE

The purpose of this report is to analyze stormwater designs for Lomas Del Sur and Cuatro Vientos Sur Subdivisions. The intent of this analysis is to determine if the proposed channel and detention pond for Lomas Del Sur can accommodate the post development flow from Cuatro Vientos Sur Subdivision.

By conveying post flow through Lomas Del Sur drainage system, a detention pond can be eliminated within Cuatro Vientos Sur thus reducing long term maintenance costs for the Webb County Drainage District. Stormwater designs for each subdivision were provided by the respective consultant engineers representing the developer. Refer to Exhibit 1 for Location Map.

This report does not attempt to confirm that the subdivision designs are in compliance to the City of Laredo Land Development Code as it is understood that the developer and its consultant has addressed all requirements.

2. EXISTING CONDITIONS

Cuatro Vientos Subdivision is located upstream from Lomas Del Sur Subdivision. Its watershed is 169.59 acres or 30.5% of the total watershed while Lomas Del Sur watershed totals 386.44 acres or 69.5% of the total. For the purpose of this analysis, the watershed is being identified as A1.

Watershed A1 is comprised of approximately 556 acres and is bound on the north by Cuatro Vientos Norte Subdivision, the west by Ejido Avenue, the south by Pita Mangana Road, and the east by Cuatro Vientos Rd. Small areas of the watershed exceed the bounding roads. The watershed includes developed and undeveloped land both within the Laredo City limits.

There are two (2) tributaries that convey stormwater and converge at an existing pond adjacent to Ejido Avenue. Pond discharges through a natural creek and leaves the property along Ejido along its natural course. The two tributaries are stream order 1 creeks and the creek at the downstream side of the pond is a 2nd order stream. There are currently no effective special flood hazard areas within the watershed being studied. Exhibit 2 illustrates existing creek system.

The overall watershed is composed of two (2) types of soils that contain hydrologic properties that vary from being in groups B-D as depicted in Exhibit 3 Soils Map according to the NRCS Soil Survey of Webb County, Texas. The project site consists of Verick Fine Sandy Loam (VkC) and Copita (CpB). The descriptions of these soils are as follows:

VkC – Verick Fine Sandy Loam (VkC)-This soil is well drained. Surface runoff is medium, and permeability is moderate. Water erosion and soil blowing are moderate hazards if this soil is left bare of vegetation. This soil is poorly suited to most urban and recreation uses. Shallowness to sandstone is the main limitation. This soil is in the Shallow Sandy Loam range site.

CpB – Copita fine sandy loam- This moderately deep, nearly level to gently sloping soil is on summits and side slopes of low hills and on broad, convex plains. Typically, the surface layer is brown fine sandy loam about 9 inches thick. Water erosion and soil blowing are moderate hazards if this soil is left bare of vegetation. This soil is moderately well suited to most urban uses.

3. PROPOSED MASTERPLANS

Proposed Masterplans were provided by the developers for both Lomas Del Sur and Cuatro Vientos Sur Subdivisions. Refer to Exhibits 4 and 5 for Masterplans. Currently, the extension of Lomas Del Sur Blvd. is ongoing with construction of a culvert crossing to be incorporated into this analysis. Through coordination with TxDOT, design plans and criteria were made available to us for integration into the effective models developed and discussed further in Section 4 – H&H Analysis.

The Lomas Del Sur Masterplan proposes various landuses such as commercial, singlefamily residential, multi-family residential, and a future school site. Lomas Del Sur's drainage masterplan indicates one major channel system within a proposed 120' Drainage Easement and one detention pond site of approximately 8.67 acres. Preliminary design plans call for an approximate 2,332 LF of earthen channel beginning from the southern boundary of the proposed development to the proposed pond site with 14' bottom width, 6:1 side slopes, 74' top of channel, 5' depth, and a 20' access road within the easement. The detention pond shown on the provided preliminary plat for Lomas Del Sur displays a pond depth of approximately 17' determined from the contours on said plat. This development's drainage masterplan includes watersheds which do incorporate the neighboring Cuatro Vientos Sur, and are consistant with our watershed area.

The TxDOT designed culvert crossing lying intermediately within the proposed Lomas Del Sur drainage channel consists of three (3) 127 LF runs of 48" diameter reinforced concrete pipe accounting for a 256.10 acre drainage area. According to construction plans for this structure, a 10 year design flow of 270.35 cfs was utilized to design this improvement.

Porras-Nance Engineering provided their drainage masterplan for Cuatro Vientos Sur consisting of a short pilot channel and detention pond site roughly 3.58 acres in size. The masterplan indicates proposed landuses include commercial, single-family residential, multi-family residential and a future school site. As stated in the purpose, it is the intent of this analysis to remove the need for detention for this subdivision. The proposed channel design provided is comprised of an 8' wide, 1' deep pilot channel, 14' gross bottom width, 3:1 side slopes, 40' top width, and 4.33' foot depth within a 70' wide drainage easement.

The contributing watersheds as per the masterplan accrue to an approximate 168.81 acres in which sub-watershed A1-A of this analysis is comparable at 169.59 acres.

4. H&H ANALYSIS

A feasibility study for the two cooperating developments described in the previous section consisting of a H&H Analysis was prepared by integrating these proposed developments to determine if individual detention ponds can be replaced with a regional pond.

Exhibit 6 provides watershed delineations used to estimate time of concentration. The SCS Curve Method was utilized to develop design flows. Pre-development and post-development flows take into consideration hydrologic soil types, current and future landuse, proposed drainage designs provided by respective engineering consultants, antecedent moisture conditions, and existing storm drainage structures.

As per the future masterplans provided, channels were analyzed for adequate capacity in conveyance of post development flow. Post and predevelopment flows are indicated for 10-year, 25-year, and 50-year return events. Flows determined within this analysis for Watershed A1 are as follows:

Comparing Watershed A1, totaling 556 acres, flows for the 25-year event (1696.79 cfs) to Sherfey's calculations (1833 cfs for 552 acres) indicates some variance in our approach which can be attributed to our integration of antecedent moisture conditions in determining SCS Curve Numbers and the delineation of various smaller sub-watersheds by Sherfey Engineering. For the purpose of this analysis, a design flow of 1765 cfs for a 25-year event is being utilized.

Sub-watershed A1-A is comprised of Cuatro Vientos Sur's contributing watershed. Porras-Nance Engineering's contributing watershed measures 168.81 acres in comparison to this study sub-watershed A1-A delineated at 169.59 acres. The design flow for the proposed pilot channel for Cuatro Vientos Sur is 520 cfs, while the 25-year post development flow determined for A1-A is 517.52 cfs. This comparison of watershed areas indicate the same area however reviewing Porras-Nance, Sherfey, and our study, the following design flows for a 25-year post development flow are compared:

| Porras-Nance | Sherfey | Crane |
|--------------|---------|---------|
| 806 cfs | 630 cfs | 518 cfs |

Porras-Nance utilizes the rational method for computing this runoff and also provides a separate design flow of 520 cfs for their pilot channel design (Exhibit 7). Sherfey and Crane utilize the SCS curve method with Sherfey's flow higher due to smaller watersheds in their analysis. Based on this information, a design flow of 600 cfs is being utilized for this analysis.

H&H Run Results (Exhibit 8)

HEC-RAS, HY-8, and Pondpack were utilized to model the estimated flows for Cuatro Vientos Sur and Lomas Del Sur. Models were developed utilizing plans received from Lomas consultants on 10/20/14 and 10/17/14, Cuatro Vientos consultants on 10/10/14, and TxDOT. The following observations are made based on these designs as follows:

- A1: The first run of channel from Cuatro Vientos Sur Lomas Del Sur common line up to 500 ft south of the recently constructed Lomas Del Sur drainage crossing is able to accommodate the estimated flow of both developments. The only drawback is the velocity in this channel segment exceeds 5 ft/sec. This will require improvements to combat the high velocity.
- A2: The channel overtops its banks as flow approaches the drainage crossing at Lomas Del Sur which is undersized and creates a backwater effect that causes this overtopping effect. Flow also overtops Lomas Del Sur Boulevard which is currently under construction. Review of construction plans indicate drainage crossing design is base on a 10 year pre development flow.
- A3: The channel downstream of Lomas Del Sur crossing to proposed detention pond accommodates the flow released by the drainage crossing but velocities along channel exceed 5 ft/sec.
- B1: The second run of the channel design which provides drop structures produces similar results as the first run. Higher velocities are reduced and are confined to the drop structure section. Runoff overtops Lomas Del Sur Boulevard and velocities within the channel downstream of the Lomas crossing exceed 5 ft/sec.
- C1: The maximum flow that the drainage crossing at Lomas Del Sur Boulevard can support and still provide a one (1') freeboard to the top of headwall is 400 cfs.
- D1: The Lomas Del Sur pond provides adequate storage (81.33 ac/ft) of post development runoff for both developments maintaining adherence to City ordinance releasing less than predevelopment flow for each storm event.

| Return Event | Predevelopment Runoff | Computed Outflow | Freeboard |
|--------------|--------------------------|------------------|-----------|
| 50 year | 1,140.58 cfs | 851.31 cfs | 2.72 ft |
| 25 year | 883.28 cfs | 766.78 cfs | 4.61 ft |
| 10 year | 618.24 cfs | 620.49 cfs | 7.4 ft |
| | | | |

5. CONCLUSIONS & RECOMMENDATIONS

The overall plan developed by Lomas Del Sur consultants is adequate to support Cuatro Vientos Sur post development flow as well as Lomas Del Sur post flow. This plan fails at the Lomas Del Sur Boulevard drainage crossing recently constructed under a joint project by TxDOT and City of Laredo.

As a result, the elimination of a detention pond at Cuatro Vientos Sur is not feasible. It is recommended that Cuatro Vientos construct a detention pond within its development and reevaluate its outlet design flow as the Lomas Del Sur drainage crossing has a maximum estimated capacity of 400 cfs.

Lomas Del Sur must also reevaluate its stormwater masterplan to address the flow restrictions at Lomas Del Sur Boulevard. This limitation will not allow the downstream pond to effectively serve the development and might require Lomas developers to develop an additional detention pond upstream of the Lomas Del Sur Boulevard drainage crossing.

Another option would be for the Cuatro Vientos Sur development to add additional pipes at the Lomas Del Sur crossing to increase flow under the road in order to eliminate need for detention pond. This would be subject to Lomas Del Sur willingness to accept Cuatro Vientos Sur post flow.







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LOMAS DEL SUR MASTERPLAN

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N

DEVELOPED CONDITIONS Date: 2/20/2006

MASTER DRAINAGE PLAN LOMAS DEL SUR

BASE MAP IS TAKEN FROM UNITED STATES DEPARTMENT OF INTEROR, GEOLOGICAL SURVEY, LAREDO SOUTH QUADRAVIGE, DATED 1979. 7.5 MINUTE SERIES (TOPOGRAPHIC)

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| ns | 764 | 79 | 65 | 635 | 142 | 196 | 138 | 662 | 541 | 490 | Develop Return Pe 25 yr | F ANAL |
| | 850 | 101 | 81 | 732 | 169 | 231 | 163 | 795 | 651 | 590 | conditions rlod (CFS) 50 yr | SISL |
| | 943 | 127 | 102 | 847 | 200 | 263 | 193 | 958 | 784 | 713 | 100 yr | |

| 471.00 8.6 | 466.00 7.3 | 460.00 5.9 | 455.50 5.0 | Elevation An (ft) (ac | |
|-------------|--------------------------|--------------------------|--|-------------------------------------|----------------|
| 7 25.52 8 | 5 21.22 1 5 23.48 3 | 3 19.07 2 | 5 15.70 1 | ea A1+A2+sqr(A1" res) (acres) | PROPOSED |
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| nese areas | .35 | 0.49 0.37 | 0.60 0.61 0.31 | | 0.32 | 0.53 | 0.56 | 0.62 | 0.48 | 0.42 | 0.46 | - | 0.39 | - | 1.15 | 0.29 | 0.19 | 0.26 | 1.10 | 70 | | Dev |
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СрВ √кС J. EGEND PROPOSED FLOW EXISTING FLOW WATERSHED DELINEATION PROPOSED FLOW ON STREETS 50 FT CONTOURS

COPITA B (hydrological soil type) VERICK C (hydrological soil type)

PROJ. NO. 8036.0.



| D.A. | с | I ₁₀ | A (ac.) | Q ₁₀ (cfs) | Proposed Use | D.A. | с | I ₁₀ | A (ac.) | Q ₁₀ (cfs) |
|------|------|-----------------|---------|-----------------------|--------------------------------------|------|------|-----------------|---------|-----------------------|
| А | 0.35 | 4.01 | 73.92 | 103.75 | Commercial | А | 0.95 | 5.81 | 11.81 | 65.19 |
| в | 0.35 | 4.73 | 86.48 | 143.17 | Residential/Commercial/Institutional | в | 0.70 | 5.90 | 157.00 | 648.41 |
| с | 0.35 | 6.79 | 11.83 | 28.11 | Residential | с | 0.52 | 6.42 | 5.80 | 19.36 |
| D | 0.35 | 5.17 | 13.92 | 25.19 | Residential / Commercial | D | 0.81 | 5.72 | 15.64 | 72.46 |
| Е | 0.35 | 5.03 | 14.54 | 25.60 | Residential / Commercial | Е | 0.66 | 4.97 | 14.32 | 46.97 |
| F | 0.35 | 5.12 | 3.27 | 5.86 | Institutional | F | N/A | N/A | N/A | N/A |

| D.A. | с | I ₂₅ | A (ac.) | Q ₂₅ (cfs) | Proposed Use | D.A. | с | I ₅₀ | A (ac.) | Q ₅₀ (cfs) |
|------|------|-----------------|---------|-----------------------|--------------------------------------|------|------|-----------------|---------|-----------------------|
| А | 0.95 | 6.57 | 11.81 | 73.71 | Commercial | A | 0.95 | 7.29 | 11.81 | 81.79 |
| в | 0.70 | 6.67 | 157.00 | 733.03 | Residential/Commercial/Institutional | в | 0.70 | 7.41 | 157.00 | 814.36 |
| с | 0.52 | 7.24 | 5.80 | 21.84 | Residential | с | 0.52 | 8.03 | 5.80 | 24.22 |
| D | 0.81 | 6.47 | 15.64 | 81.96 | Residential / Commercial | D | 0.81 | 7.18 | 15.64 | 90.96 |
| E | 0.66 | 5.64 | 14.32 | 53.30 | Residential / Commercial | E | 0.66 | 6.27 | 14.32 | 59.26 |

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OFTICE (956) 724-309 FAX (956) 724-920

AND CALCULATIONS

DETENTION POND

PONDPACK

MASTER SUMMARY



Catchments Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (hours) | Peak Flow (ft ³ /s) |
|--------------|-----------------------------|----------------------------|------------------------------|-------------------------|-----------------------------------|
| Watershed A1 | Pre-Development 10 year | 10 | 87.324 | 12.400 | 618.24 |
| Watershed A1 | Post-Development 10 year | 10 | 157.085 | 12.300 | 1,328.56 |
| Watershed A1 | Pre-Development 25 year | 25 | 120.373 | 12.400 | 883.28 |
| Watershed A1 | Post-Development 25 year | 25 | 200.398 | 12.300 | 1,696.79 |
| Watershed A1 | Pre-Development 50 year | 50 | 152.688 | 12.400 | 1,140.58 |
| Watershed A1 | Post-Development 50 year | 50 | 240.995 | 12.300 | 2,037.69 |

Node Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (hours) | Peak Flow (ft ³ /s) |
|-------|-----------------------------|----------------------------|------------------------------|-------------------------|-----------------------------------|
| J-3 | Pre-Development 10 year | 10 | 87.324 | 12.400 | 618.24 |
| J-3 | Post-Development 10 year | 10 | 157.085 | 12.300 | 1,328.56 |
| J-3 | Pre-Development 25 year | 25 | 120.373 | 12.400 | 883.28 |
| J-3 | Post-Development 25 year | 25 | 200.398 | 12.300 | 1,696.79 |
| J-3 | Pre-Development 50 year | 50 | 152.688 | 12.400 | 1,140.58 |
| J-3 | Post-Development 50 year | 50 | 240.995 | 12.300 | 2,037.69 |
| O-1 | Pre-Development 10 year | 10 | 83.060 | 12.950 | 301.48 |
| O-1 | Post-Development 10 year | 10 | 151.938 | 12.750 | 620.49 |
| O-1 | Pre-Development 25 year | 25 | 115.363 | 12.900 | 453.77 |
| O-1 | Post-Development 25 year | 25 | 201.547 | 12.750 | 766.78 |
| O-1 | Pre-Development 50 year | 50 | 147.100 | 12.900 | 570.70 |
| O-1 | Post-Development 50 year | 50 | 241.866 | 12.800 | 851.31 |

Pond Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (hours) | Peak Flow (ft³/s) | Maximum Water Surface Elevation (ft) | Maximum Pond Storage (ac-ft) |
|------------|---------------------------------|----------------------------|---------------------------------|-------------------------|----------------------|---|------------------------------------|
| PO-3 (IN) | Pre-Development 10 year | 10 | 87.282 | 12.450 | 617.55 | (N/A) | (N/A) |
| PO-3 (OUT) | Pre-Development 10 year | 10 | 83.060 | 12.950 | 301.48 | 464.86 | 23.591 |
| PO-3 (IN) | Post- Development 10 year | 10 | 157.029 | 12.350 | 1,317.52 | (N/A) | (N/A) |
| PO-3 (OUT) | Post- Development 10 year | 10 | 151.938 | 12.750 | 620.49 | 468.60 | 47.174 |
| PO-3 (IN) | Pre-Development 25 year | 25 | 120.320 | 12.450 | 878.78 | (N/A) | (N/A) |
| PO-3 (OUT) | Pre-Development 25 year | 25 | 115.363 | 12.900 | 453.77 | 466.32 | 32.413 |
| PO-3 (IN) | Post- Development 25 year | 25 | 207.260 | 12.250 | 2,692.91 | (N/A) | (N/A) |
| PO-3 (OUT) | Post- Development 25 year | 25 | 201.547 | 12.750 | 766.78 | 471.39 | 66.920 |
| PO-3 (IN) | Pre-Development 50 year | 50 | 152.624 | 12.450 | 1,132.04 | (N/A) | (N/A) |
| PO-3 (OUT) | Pre-Development 50 year | 50 | 147.100 | 12.900 | 570.70 | 467.81 | 41.932 |
| PO-3 (IN) | Post- Development 50 year | 50 | 248.141 | 12.150 | 2,692.91 | (N/A) | (N/A) |
| PO-3 (OUT) | Post- Development 50 year | 50 | 241.866 | 12.800 | 851.31 | 473.28 | 81.330 |

Subsection: Time of Concentration Calculations Label: LDS

Time of Concentration Results

| Segment #1: TR-55 Shallow Concentrated Flow | | | | | |
|---|-------------|--|--|--|--|
| Hydraulic Length | 2,692.00 ft | | | | |
| Is Paved? | True | | | | |
| Slope | 0.020 ft/ft | | | | |
| Average Velocity | 2.87 ft/s | | | | |
| Segment Time of Concentration | 0.260 hours | | | | |

Return Event: Post Development

| Segment #2: TR-55 C | hannel Flow | | | |
|--------------------------------------|-----------------|-----------------------|--|--|
| Flow Area | | 24.5 ft ² | | |
| Hydraulic Length | | 495.00 ft | | |
| Manning's n | | 0.016 | | |
| Slope | | 0.003 ft/ft | | |
| Wetted Perimeter | | 24.67 ft | | |
| Average Velocity | | 5.41 ft/s | | |
| Segment Time of Conce | ntration | 0.025 hours | | |
| Segment #3: TR-55 C | hannel Flow | | | |
| Flow Area | | 267.0 ft ² | | |
| Hydraulic Length | | 2,803.00 ft | | |
| Manning's n | | 0.035 | | |
| Slope | | 0.005 ft/ft | | |
| Wetted Perimeter | | 90.00 ft | | |
| Average Velocity | | 5.90 ft/s | | |
| Segment Time of Conce | ntration | 0.132 hours | | |
| Segment #4: Length a | and Velocity | | | |
| Hydraulic Length | | 105.00 ft | | |
| Velocity | | 10.00 ft/s | | |
| Segment Time of Conce | ntration | 0.003 hours | | |
| Time of Concentration | (Composite) | | | |
| Time of Concentration (Composite) | | 0.421 hours | | |
| ==== User Define | d Length & | Velocity | | |
| Tc = | (Lf / V) / 3600 |) | | |
| | Tc= Time of c | concentration, hours | | |
| Where: | Lf= Flow lengt | th, feet | | |
| | V= Velocity, ft | t/sec | | |
| | Shallow Co | ncontration Flow | | |
| | | | | |

S TR-55 Shallow Concentration Flow

| | Unpaved surface: V = 16.1345 * (Sf**0.5) |
|--------|---|
| Tc = | Paved Surface: V = 20.3282 * (Sf**0.5) |
| Where: | (Lf / V) / 3600 V= Velocity, ft/sec Sf= Slope, ft/ft Tc= Time of concentration, hours Lf= Flow length, feet |

==== SCS TR-55 Sheet Flow

| Tc = | (0.007 * ((n * Lf)**0.8)) / ((P**0.5) * (Sf**0.4)) |
|--------|--|
| | Tc= Time of concentration, hours |
| | n= Manning's n |
| Where: | Lf= Flow length, feet |
| | P= 2yr, 24hr Rain depth, inches |
| | Sf= Slope, % |
| | |

Label: LDS

Time of Concentration Results

| Segment #1: TR-55 Shallow Concentrated Flow | | | | | |
|---|----------------------|--|--|--|--|
| Hydraulic Length | 1,872.00 ft | | | | |
| Is Paved? | True | | | | |
| Slope | 0.020 ft/ft | | | | |
| Average Velocity | 2.87 ft/s | | | | |
| Segment Time of Concentration | 0.181 hours | | | | |
| Segment #2: Length and Velocity | | | | | |
| Hydraulic Length | 105.00 ft | | | | |
| Velocity | 10.00 ft/s | | | | |
| Segment Time of Concentration | 0.003 hours | | | | |
| Segment #3: TR-55 Channel Flow | | | | | |
| Flow Area | 24.5 ft ² | | | | |
| Hydraulic Length | 3,623.00 ft | | | | |
| Manning's n | 0.035 | | | | |
| Slope | 0.005 ft/ft | | | | |
| Wetted Perimeter | 24.67 ft | | | | |
| Average Velocity | 2.84 ft/s | | | | |
| Segment Time of Concentration | 0.354 hours | | | | |
| Time of Concentration (Composite) | | | | | |
| Time of Concentration (Composite) | 0.538 hours | | | | |
| ==== User Defined Length & Velocity | | | | | |

$\begin{array}{ll} {\sf Tc}=& & (Lf \ / \ V) \ / \ 3600 \\ {\sf Tc}= \ {\sf Time} \ of \ concentration, \ hours \\ {\sf Where:} & {\sf Lf}= \ {\sf Flow} \ {\sf length}, \ {\sf feet} \\ {\sf V}= \ {\sf Velocity}, \ {\sf ft/sec} \end{array}$

==== SCS TR-55 Shallow Concentration Flow

| Unp | aved | surf | ac | e: | | |
|-----|------|------|----|------|-----|----|
| V = | 16.1 | 345 | * | (Sf* | *0. | 5) |

Tc =

Paved Surface: V = 20.3282 * (Sf**0.5)

(Lf / V) / 3600 V= Velocity, ft/sec Sf= Slope, ft/ft Tc= Time of concentration, hours Lf= Flow length, feet

==== SCS TR-55 Sheet Flow

| Tc = | (0.007 * ((n * Lf)**0.8)) / ((P**0.5) * (Sf**0.4)) |
|--------|--|
| | Tc= Time of concentration, hours |
| | n= Manning's n |
| Where: | Lf= Flow length, feet |
| | P= 2yr, 24hr Rain depth, inches |
| | Sf= Slope, % |

Return Event: Pre-Development

Subsection: Runoff CN-Area Label: LDS Return Event: Post Development

Runoff Curve Number Data

| Soil/Surface Description | CN | Area | С | UC | Adjusted CN |
|--|--------|---------|-------|-------|-------------|
| | | (acres) | (%) | (%) | |
| Impervious Areas - Paved; curbs and storm sewers - Soil B | 95.000 | 9.560 | 0.0 | 0.0 | 95.000 |
| Impervious Areas - Paved; curbs and storm sewers - Soil C | 95.000 | 23.450 | 0.0 | 0.0 | 95.000 |
| Residential Districts - 1 acre - Soil C | 70.000 | 194.840 | 0.0 | 0.0 | 70.000 |
| Residential Districts - 1 acre - Soil B | 60.000 | 75.130 | 0.0 | 0.0 | 60.000 |
| Urban Districts - Commercial & Business - Soil B | 87.000 | 7.250 | 0.0 | 0.0 | 87.000 |
| Urban Districts - Commercial & Business - Soil C | 90.000 | 52.900 | 0.0 | 0.0 | 90.000 |
| Residential Districts - 1/8 acre (town houses) - Soil B | 78.000 | 9.070 | 0.0 | 0.0 | 78.000 |
| Residential Districts - 1/8 acre (town houses) - Soil C | 85.000 | 16.760 | 0.0 | 0.0 | 85.000 |
| Residential- Soil B | 60.000 | 32.770 | 0.0 | 0.0 | 60.000 |
| Residential- Soil C | 70.000 | 96.660 | 0.0 | 0.0 | 70.000 |
| School Site- Soil B | 60.000 | 10.490 | 0.0 | 0.0 | 60.000 |
| School Site - Soil C | 70.000 | 27.150 | 0.0 | 0.0 | 70.000 |
| COMPOSITE AREA & WEIGHTED CN> | (N/A) | 556.030 | (N/A) | (N/A) | 72.062 |

Subsection: Runoff CN-Area Label: LDS

Return Event: Pre Development

Runoff Curve Number Data

| Soil/Surface Description | CN | Area | C (%) | UC | Adjusted CN |
|---------------------------------------|--------|---------|----------|-------|-------------|
| Open space (Lawns,parks etc.) - Good | E2 000 | (dcies) | (70) | (70) | E2 000 |
| condition; grass cover > 75% - Soil B | 52.000 | 400.150 | 0.0 | 0.0 | 52.000 |
| Open space (Lawns,parks etc.) - Good | 65.000 | 155.880 | 0.0 | 0.0 | 65.000 |
| COMPOSITE AREA & WEIGHTED CN> | (N/A) | 556.030 | (N/A) | (N/A) | 55.644 |

Index

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LDS (Time of Concentration Calculations, 25 years)...3, 4, 5, 6

М

Master Network Summary...1, 2

WCDD Mapping(LDS).ppc 10/28/2014

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L



| HEC-RAS | Plan: Drop Structures | River: LDS | Reach: 1 |
|---------|-----------------------|------------|----------|
|---------|-----------------------|------------|----------|

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|-------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| 1 | 2332.54 | 10 yr | 489.00 | 502.00 | 505.39 | | 505.66 | 0.003642 | 4.21 | 116.20 | 54.63 | 0.51 |
| 1 | 2332.54 | 25 yr | 600.00 | 502.00 | 505.70 | | 506.01 | 0.003725 | 4.48 | 134.04 | 58.42 | 0.52 |
| 1 | 2332.54 | 50 yr | 704.00 | 502.00 | 505.96 | | 506.31 | 0.003802 | 4.70 | 149.75 | 61.56 | 0.53 |
| | | | | | | | | | | | | |
| 1 | 2219.84 | 10 yr | 489.00 | 501.66 | 504.05 | 504.05 | 504.86 | 0.015742 | 7.21 | 67.85 | 42.71 | 1.01 |
| 1 | 2219.84 | 25 yr | 600.00 | 501.66 | 504.32 | 504.32 | 505.20 | 0.015298 | 7.53 | 79.64 | 45.91 | 1.01 |
| 1 | 2219.84 | 50 yr | 704.00 | 501.66 | 504.54 | 504.54 | 505.49 | 0.014956 | 7.80 | 90.31 | 48.62 | 1.01 |
| | | | | | | | | | | | | |
| 1 | 1899.03 | 10 yr | 489.00 | 492.04 | 495.47 | | 495.73 | 0.003455 | 4.13 | 118.48 | 55.13 | 0.50 |
| 1 | 1899.03 | 25 yr | 600.00 | 492.04 | 495.78 | | 496.08 | 0.003547 | 4.40 | 136.50 | 58.92 | 0.51 |
| 1 | 1899.03 | 50 yr | 704.00 | 492.04 | 496.05 | | 496.38 | 0.003617 | 4.62 | 152.54 | 62.10 | 0.52 |
| | | | | | | | | | | | | |
| 1 | 1769.84 | 10 yr | 489.00 | 491.65 | 494.04 | 494.04 | 494.85 | 0.015743 | 7.21 | 67.85 | 42.71 | 1.01 |
| 1 | 1769.84 | 25 yr | 600.00 | 491.65 | 494.31 | 494.31 | 495.19 | 0.015300 | 7.53 | 79.64 | 45.91 | 1.01 |
| 1 | 1769.84 | 50 yr | 704.00 | 491.65 | 494.53 | 494.53 | 495.48 | 0.014953 | 7.79 | 90.32 | 48.62 | 1.01 |
| | | | | | | | | | | | | |
| 1 | 1619.84 | 10 yr | 489.00 | 487.15 | 490.74 | 489.54 | 490.97 | 0.002830 | 3.83 | 127.55 | 57.07 | 0.45 |
| 1 | 1619.84 | 25 yr | 600.00 | 487.15 | 491.07 | 489.81 | 491.33 | 0.002910 | 4.09 | 146.87 | 61.00 | 0.46 |
| 1 | 1619.84 | 50 yr | 704.00 | 487.15 | 491.34 | 490.03 | 491.63 | 0.002976 | 4.29 | 163.98 | 64.28 | 0.47 |
| | | | | | | | | | | | | |
| 1 | 1405.03 | 10 yr | 489.00 | 486.51 | 488.90 | 488.90 | 489.71 | 0.015742 | 7.21 | 67.85 | 42.71 | 1.01 |
| 1 | 1405.03 | 25 yr | 600.00 | 486.51 | 489.17 | 489.17 | 490.05 | 0.015315 | 7.54 | 79.61 | 45.90 | 1.01 |
| 1 | 1405.03 | 50 yr | 704.00 | 486.51 | 489.40 | 489.40 | 490.34 | 0.014919 | 7.79 | 90.40 | 48.64 | 1.01 |
| | | | | | | | | | | | | |
| 1 | 1219.84 | 10 yr | 489.00 | 480.95 | 487.26 | | 487.30 | 0.000202 | 1.54 | 316.95 | 74.00 | 0.13 |
| 1 | 1219.84 | 25 yr | 600.00 | 480.95 | 487.77 | | 487.81 | 0.000213 | 1.69 | 354.49 | 74.00 | 0.14 |
| 1 | 1219.84 | 50 yr | 704.00 | 480.95 | 488.18 | | 488.23 | 0.000225 | 1.83 | 385.13 | 74.00 | 0.14 |
| | | | | | | | | | | | | |
| 1 | 902.43 | 10 yr | 722.00 | 480.00 | 487.17 | | 487.22 | 0.000247 | 1.90 | 380.38 | 74.00 | 0.15 |
| 1 | 902.43 | 25 yr | 898.00 | 480.00 | 487.66 | | 487.73 | 0.000286 | 2.16 | 416.60 | 74.00 | 0.16 |
| 1 | 902.43 | 50 yr | 1062.00 | 480.00 | 488.05 | | 488.14 | 0.000323 | 2.38 | 445.97 | 74.00 | 0.17 |

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|-------|-----------|---------|---------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| | | | | | | | | | | | | |
| 1 | 750 | 10 yr | 722.00 | 478.80 | 487.15 | 481.72 | 487.19 | 0.000128 | 1.54 | 468.21 | 74.00 | 0.11 |
| 1 | 750 | 25 yr | 898.00 | 478.80 | 487.64 | 482.07 | 487.69 | 0.000157 | 1.78 | 504.25 | 74.00 | 0.12 |
| 1 | 750 | 50 yr | 1062.00 | 478.80 | 488.04 | 482.36 | 488.10 | 0.000185 | 1.99 | 533.43 | 74.00 | 0.13 |
| 1 | 683.16 | | Culvert | | | | | | | | | |
| 1 | 619 | 10 yr | 722.00 | 477.84 | 482.18 | | 482.45 | 0.002665 | 4.15 | 174.05 | 66.13 | 0.45 |
| 1 | 619 | 25 yr | 898.00 | 477.84 | 482.70 | | 482.98 | 0.002496 | 4.28 | 209.72 | 72.31 | 0.44 |
| 1 | 619 | 50 yr | 1062.00 | 477.84 | 483.12 | | 483.42 | 0.002306 | 4.42 | 240.43 | 74.00 | 0.43 |
| 1 | 604 | 10 yr | 1054.00 | 477.63 | 481.18 | 481.18 | 482.28 | 0.013859 | 8.43 | 125.08 | 56.55 | 1.00 |
| 1 | 604 | 25 yr | 1322.00 | 477.63 | 481.57 | 481.57 | 482.80 | 0.013715 | 8.90 | 148.49 | 61.32 | 1.01 |
| 1 | 604 | 50 yr | 1571.00 | 477.63 | 481.93 | 481.93 | 483.24 | 0.013160 | 9.17 | 171.36 | 65.64 | 1.00 |
| 1 | 550 | 10 yr | 1054.00 | 476.86 | 480.40 | 480.40 | 481.51 | 0.013880 | 8.43 | 125.01 | 56.54 | 1.00 |
| 1 | 550 | 25 yr | 1322.00 | 476.86 | 480.80 | 480.80 | 482.03 | 0.013704 | 8.90 | 148.53 | 61.33 | 1.01 |
| 1 | 550 | 50 yr | 1571.00 | 476.86 | 481.16 | 481.16 | 482.47 | 0.013173 | 9.17 | 171.30 | 65.63 | 1.00 |
| | | | | | | | | | | | | |
| 1 | 0 | 10 yr | 1054.00 | 469.00 | 472.54 | 472.54 | 473.65 | 0.013910 | 8.44 | 124.91 | 56.51 | 1.00 |
| 1 | 0 | 25 yr | 1322.00 | 469.00 | 472.94 | 472.94 | 474.17 | 0.013734 | 8.91 | 148.41 | 61.30 | 1.01 |
| 1 | 0 | 50 yr | 1571.00 | 469.00 | 473.30 | 473.30 | 474.61 | 0.013193 | 9.18 | 171.21 | 65.61 | 1.00 |

HEC-RAS Plan: Drop Structures River: LDS Reach: 1 (Continued)



HY – 8 CULVERT ANALYSIS

| Discharge Names | Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | Inlet Control Depth (ft) | Outlet Control Depth (ft) | Flow ⊤ype | Normal Depth (ft) | Critical Depth (ft) | Outlet Depth (ft) | Tailwater Depth (ft) | Outlet Velocity (ft/s) |
|-------------------------|-----------------------------|-------------------------------|-----------------------------|-----------------------------|---------------------------------|--------------|----------------------|------------------------|----------------------|-------------------------|------------------------------|
| TxDOT 10 yr Pre | 280.00 | 280.00 | 483.69 | 4.875 | 0.238 | 5-S2n | 2.425 | 2.925 | 2.497 | 1.218 | 11.328 |
| Max with Freeboard | 400.00 | 400.00 | 485.92 | 7.103 | 6.292 | 5-S2n | 3.207 | 3.445 | 3.219 | 1.497 | 12.337 |
| LDS/CVS 25 _yr Post_ | 898.00 | 515.55 | 488.90 | 10.079 | 8.799 | 7-M2c | 4.000 | 3.735 | 3.735 | 2.372 | 14.075 |

 Table 2 - Culvert Summary Table: Lomas Del Sur Crossing

Water Surface Profile Plot for Culvert: Lomas Del Sur Crossing



Site Data - Lomas Del Sur Crossing

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 478.82 ft Outlet Station: 127.00 ft Outlet Elevation: 477.84 ft Number of Barrels: 3

Culvert Data Summary - Lomas Del Sur Crossing

Barrel Shape: Circular Barrel Diameter: 4.00 ft Barrel Material: Concrete Embedment: 0.00 in Barrel Manning's n: 0.0120 Culvert Type: Straight Inlet Configuration: Square Edge with Headwall Inlet Depression: NONE

PONDPACK

PONDMAKER Worksheet Report



| Element Details | | | |
|-----------------------------|------------------------|--|-------------|
| ID | 104 | | |
| Label | Worksheet | (PO-3) - 1 | |
| Select Pond to Design | PO-3 | | |
| Flow Allowed Below Target | 25.0 | | |
| Flow Allowed Above Target | 0.0 | | |
| Flow Allowed Below Target | 30.0 | | |
| Flow Allowed Above Target | 0.0 | | |
| Volume Allowed Below Target | 25.0 | | |
| Volume Allowed Above Target | 50.0 | | |
| Tolerance Display | Display PAS | SS for values within specified tolerance | |
| Notes | | | |
| Volume | | | |
| Pond Type | Elevation- Area | Use Void Space? | False |
| E | levation-Area | | |
| | | | |
| Pond Elevation (ft) | | Pond Area (acres) | |
| | 460.50 | 5.020 | |
| | 463.00 | 5.450 | |
| | 465.00 | 5.900 | |
| | 469.00 | 6.830 | |
| | 471.00 | 7.320 | |
| | 475.00 | 8.350 | |
| | 476.00 | 8.670 | |
| Infiltration | | | |
| Infiltration Method | No Infiltration | | |
| Output | | | |
| Detention Time | Compute All Methods | | |
| Initial Conditions | | | |
| Is Outflow Averaging On? | False | Define Starting Water Surface Elevation | Pond Invert |

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| Design Scenario I | | | Design Return Event | Target Pea Outflow (ft³/s) | ak T V V | Farget Outflow Yolume Gac-ft) | Peak Pond Inflow (ft³/s) | Total Inflow Volume (ac-ft) | | | |
|---|--|---------------------------------|---------------------------|----------------------------------|-------------------|--|---------------------------------------|-----------------------------------|--|--|--|
| Post-Developm Post-Developm Post-Developm | ent 50 year ent 25 year ent 10 year | | 50 25 10 | 1,140. 883. 618. | .58 .28 .24 | 152.688 120.373 87.324 | 2,692.9 2,692.9 1,317.5 | 1248.1411207.26052157.029 | | | |
| Estimated Storage (ac-ft) | Estimated Max Water Surface Elevation (ft) | Estimated Freeboard Depth | Design Outlet Structure | | | stimated ak Outflow (ft³/s) | Estimated Peak Outflo vs. Targe | d bw t | | | |
| 87.471 | 474.00 | Pass | Composi Structure | te Outlet e - 1 to Outlet | | 881.59 | Pass | | | | |
| 77.403 | 472.71 | Pass | Structure | e - 1 | | 826.76 | Pass | | | | |
| 58.549 | 470.23 | Pass | Composi | te Outlet e - 1 | | 709.29 | Fail | | | | |
| | | Po | ondMaker | Outlet Des | sian | | | | | | |
| 477.50 | | | | | | | | | | | |
| € ^{475.00} | | | | | | | | | | | |
| 472.50 | | | | | | | 2 | | | | |
| ຍ ສູ່ 470.00 - | | | | | | | | | | | |
| ະມັກ 467.50 - ເມັນ | | | | | | | | | | | |
| ₩ 465.00 - Puo | | | | | | | | | | | |
| ط 462.50 | | | | | | | | | | | |
| 460.00 - | L <u></u> | | | | | | | | | | |
| 0 | 0.00 | 200.00 | 400.00 | 600. Flow (ft ³ | 00 /s) | 800.00 | 1,000 |).00 | | | |
| | | | Charlos | 1 | Tarcati | otine Com | av.o | | | | |
| | Post- | Development | :10 year | - 1 - | Post-De | velopmer | nt 25 year | | | | |
| | Post-Development 50 year | | | | | | | | | | |

PondMaker Worksheet (Outlet Design)

WCDD Mapping(LDS).ppc 10/29/2014

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| D | esign Scenario | | Design Return Event | Target Peal Outflow (ft ³ /s) | c Com Peak ((ft | puted Outflow : ³ /s) | Computed Peak Outflo vs. Targe | d ow t | Target Outflow Volume (ac-ft) |
|---|--|-----------------------------------|---------------------------|--|------------------------|--|--------------------------------------|--------------|--|
| Post-Developn Post-Developn Post-Developn | nent 50 year nent 25 year nent 10 year | | 50 25 10 | 1,140.5 883.2 618.2 | 8 8 4 | 851.31 766.78 620.49 | Pass Pass Fail | | 152.688 120.373 87.324 |
| Computed Volume Outflow (ac-ft) | Computed Outflow Volume vs. Target | Routing O Structu | utlet re | Computer Max Wate Elevation (ft) | d Fre er D | eboard Pepth | Maximur Storage (ac-ft) | m e | |
| 241.866 | Fail | Composite Out Structure - 1 | let | 473. | 28 Pass | | 81.3 | 330 | |
| 201.547 | Fail | Structure - 1 | let | 471. | 39 Pass | | 66.9 | 920 | |
| 151.938 | Fail | Composite Out Structure - 1 | let | 468. | 60 Pass | | 47.: | 174 | |
| | | Pon | dMaker F | Routing Des | ign | | | | |
| 477.50 | | | | | | | | | |
| 윤 ^{475.00} | | | | | | | | | 0-01 00-00-01 01 00-01-5 |
| 472.50 | | | | | | | | | |
| ้ ยั 470.00 | | | | | | | | | |
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PondMaker Worksheet (Routing Design)

WCDD Mapping(LDS).ppc 10/29/2014

Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 Bentley PondPack V8i [08.11.01.54] Page 4 of 4